1 Quantifying the relative influence of coastal foredune growth factors on the U.S.

2 Mid-Atlantic Coast using field observations and the process-based numerical

3 model Windsurf

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17 Highlights

- 18 Pre-existing beach-dune morphology had the largest influence on dune growth
- 19 type.
- Exposure to the dominant wave direction led to increased dune volume.
- Higher minimum vegetation elevation and finer sand resulted in taller dunes.
- Minimum vegetation elevation influenced dune growth more than sand grain size.

23 Abstract

24 Coastal dunes provide many ecosystem services including protection of 25 infrastructure from wave overtopping and habitat for native species. Foredunes grow at 26 different rates and assume different forms (i.e., short and wide to tall and narrow) 27 depending on a range of factors including pre-existing beach and dune morphology, 28 wind, wave, and water levels, sediment grain size, and vegetation characteristics, yet 29 the relative importance of these factors on foredune growth is understudied. Here, we 30 quantify foredune evolution (2016-2019) and explore the relative influence of a suite of 31 metocean, sedimentary, and ecological factors for dune growth on three barrier islands 32 in the U.S. North Carolina Outer Banks (Cape Lookout National Seashore). We 33 incorporate observed and hindcast wind, wave, and water level data into the process-34 based, coupled beach-dune evolution model, Windsurf, to explore the relative 35 contribution of factors likely to influence foredune growth at the annual timescale (2016-36 2017). Our cross-shore topographic profile observations show varied interannual 37 foredune change rates and characteristics, including horizontal retreat and progradation 38 at the dune toe and vertical erosion and accretion at the dune crest. Model results 39 indicate that, of the factors explored, pre-existing morphology had the greatest influence 40 on the type of foredune growth that occurred (i.e., incipient dune development, widening 41 of the dune, and/or vertical accretion), which dramatically altered the final shape of the 42 dune. Variations in wind and wave climates were associated with the relative 43 contribution of marine- and aeolian-driven bed elevation changes and were particularly 44 influential during storms. In addition, increases in the minimum elevation of vegetation 45 on the dune profile (analogous to the cross-shore distance between the shoreline and

established vegetation line, i.e., the vegetation limit, as coined by Duran and Moore,
2013) increased dune crest height and dune volume. Moreover, variations in the
minimum vegetation elevation resulted in a larger range of dune crest elevations and
dune volumes than differences in the median sand grain size. We suggest that insights
into the relative influence of metocean, sedimentary, and ecological factors to dune
growth can assist in the development of practical coastal management strategies.

52 Keywords

53 Coastal foredune growth, dune dynamics, ecomorphodynamics, coupled beach-dune
54 modeling, sediment transport, accretion, progradation

55 **1.** Introduction

56 Coastal dunes provide a range of regulating, provisioning, cultural, and 57 supporting ecosystem services including coastal hazard protection, carbon 58 sequestration, living spaces, historical heritage, tourism, habitat for flora and fauna, and 59 nutrient cycling (Barbier et al., 2011; Martínez and Psuty, 2004; Nordstrom et al., 1989; 60 Sudmeier-Rieux et al., 2019). Dunes form, develop, and recover from storms via 61 complex ecomorphodynamic processes produced by the interactions and feedbacks 62 between metocean, sedimentary, and ecological factors (Biel et al., 2019; Charbonneau 63 et al., 2022; Corenblit et al., 2011; Durán and Moore, 2013; Hacker et al., 2019; Hesp, 64 1989; Hesp et al., 2019; Jay et al., 2022; Keijsers et al., 2016; Woodhouse, 1978; 65 Yousefi Lalimi et al., 2017; Zarnetske et al., 2015). Moreover, the rates and types of 66 coastal dune growth, including incipient dune development, widening of the dune, 67 and/or vertical accretion, are dependent on pre-existing nearshore, beach, and dune

morphology (Godfrey, 1977). Understanding the relative influence of factors influencing
dune development is important for predicting exposure to coastal hazards, improving
coastal engineering design, and informing decisions for resilient adaptation strategies
(Gracia et al., 2018; Nordstrom et al., 1989) .

72 Dune growth is primarily associated with aeolian transport of sediment from the 73 beach to the dune (Goldsmith, 1978). Controls on aeolian sediment transport include 74 the wind climate (i.e., velocity, direction, and duration) and fetch length (determined by 75 beach width), as well as the moisture content, sediment grain size distribution, and 76 topography of the beach (Bauer et al., 2009; Hoonhout and de Vries, 2016; Walker, 77 2020; White and Tsoar, 1998). Transport is typically modeled using a threshold velocity 78 approach (Bagnold, 1941), whereby wind velocities exceeding a threshold will have the 79 capacity to entrain sediment. Cross-shore transport of sediment is highest for shore-80 normal winds and is reduced for oblique winds (i.e., the cosine effect); however, oblique 81 winds result in increased fetch lengths between the waterline and dunes (Bauer and 82 Davidson-Arnott, 2003; Davidson-Arnott et al., 2018). Additionally, the concept of 83 duration-limited wind events has been proposed (Delgado-Fernandez and Davidson-84 Arnott, 2011), where a duration factor is used to regulate the amount of 'geomorphic 85 work' done by grouped wind events. The fetch length and sediment transport rate are 86 further modulated by the moisture content of the beach, which is a function of nearshore 87 processes (e.g., tidal fluctuations and runup) and rainfall events (Bauer et al., 2009). 88 Beach grain size distribution is another important factor that can govern supply 89 and transport of sand to the dune. Fine sands are more easily transported, leaving

90 coarser-grained lag on the beach surface (Bagnold, 1941; Wolner et al., 2013). Areas of

the beach that lack finer sands below the beach surface, and do not experience
hydraulic mixing from wave action, can result in lower rates of sand transport across the
beach and thus limit sediment supply to the dune (Hoonhout, 2020; Hoonhout and de
Vries, 2016). Additionally, coarser grain sizes will increase the surface roughness
length, thus reducing the threshold wind velocity (Bagnold, 1941; Belly, 1964; Field and
Pelletier, 2018).

97 Topographic characteristics such as beach slope, presence or absence of berms 98 and cusps, and dune structures themselves significantly interact with wind velocities 99 and alter bed shear stresses (Bauer et al., 1996; Jackson et al., 2013; Jackson and 100 Hunt, 1975; Sherman and Bauer, 1993; Walker and Hesp, 2013; Walker, 2020). 101 Similarly, dune vegetation increases localized drag and reduces bed shear stress, 102 resulting in sediment deposition (Charbonneau and Casper, 2018; Hesp et al., 2019; 103 Hong et al., 2019; Liu et al., 2018; Olson, 1958a; Walker and Hesp, 2013; Zarnetske et 104 al., 2012). Ecological characteristics of dunes such as vegetation abundance and 105 species composition are important determinates of dune morphology and evolution, 106 given the dual role of plants in dune-building (sand accretion) and stabilization 107 (minimizing sand loss) (Arens et al., 2001; Biel et al., 2019; Bonte et al., 2021; Bryant et 108 al., 2019; Charbonneau et al., 2021, 2017; Durán and Moore, 2013; Esler, 1970; Hacker 109 et al., 2019, 2012; Hesp, 1989; Jay et al., 2022; Keijsers et al., 2016; Olson, 1958b; 110 Seabloom et al., 2013).

Dune growth is also a function of marine processes such as waves, currents, and wave runup, which interact with the beach-dune profile and influence sediment transport gradients (Cohn et al., 2018; Hesp and Smyth, 2016; Sherman and Bauer, 1993; Short

114 and Hesp, 1982). Although marine processes clearly can have significant erosional 115 impacts on coastal foredunes, particularly during storm events (Castelle et al., 2017; 116 Komar et al., 2001; Masselink et al., 2016; Sallenger, 2000), recent studies have shown 117 that marine-driven sediment transport can also be a significant contributor to dune 118 growth (Cohn et al., 2019a, 2019b; Moulton et al., 2021). For specific hydrodynamic 119 states, i.e., high still water level and/or energetic wave periods, dune growth rates 120 driven by marine processes can be an order of magnitude larger than dune growth rates 121 driven by aeolian processes (Cohn et al., 2019a). In addition, wave climate (i.e., wave 122 height, period, and direction) can alter morphology, including the foreshore beach slope, 123 beach width, dune toe elevation, and dune crest elevation (Castelle et al., 2019; Cohn 124 et al., 2019b; Short and Hesp, 1982; Splinter et al., 2018). Likewise, morphology affects 125 wave runup processes and ultimately the effect of total water level on dune evolution 126 (Cohn et al., 2021; Gomes da Silva et al., 2020; Holman and Sallenger, 1985; 127 Sallenger, 2000; Stockdon et al., 2006). Alongshore varying wave energy also drives 128 gradients in longshore sediment transport, influencing beach sediment budgets and 129 ultimately affecting foredune growth (Miot da Silva et al., 2012; Psuty, 1988). 130 Previous studies have used field observations to explore the relative contribution

of various geological and ecological factors important to dune morphology and growth.
For example, research on the U.S. Pacific Northwest coast (Biel et al., 2019) and the
North Carolina Outer Banks (Jay et al., 2022) has shown that shoreline change rate and
beach slope were significant factors in foredune morphology and its change, while dune
grass density and species identity explained less variability. The relative influence of
these factors has also been shown to depend on the timescales over which they are

137 considered. For example, beach sand supply was found to explain more variation in
138 foredune morphology at shorter timescales (i.e., annual) while beach grass density
139 explained more variation at longer timescales (i.e., decadal) suggesting that sand
140 supply and vegetation feedbacks on dune morphology take many years to develop
141 (Zarnetske et al., 2015).

142 Field-based observational and experimental studies have revealed the 143 importance of multiple factors to dune evolution, but they are typically bound by the site-144 specific combination of factors and relatively short time scales. Process-based, beach-145 dune models provide the means for manipulating the various factors important to dune 146 morphology in a controlled manner. State-of-the-art, beach-dune models couple 147 nearshore morphodynamic and dune evolution processes to holistically simulate the full 148 coastal profile. Such models, including XBeach-Duna (Roelvink and Costas, 2019), 149 DUBEVEG (Keijsers et al., 2016), and Windsurf (Cohn et al., 2019a) provide platforms 150 to enhance our knowledge of the interdependent physical factors controlling coastal 151 dune evolution. For example, Windsurf couples XBeach (Roelvink et al., 2009), Aeolis 152 (Hoonhout and de Vries, 2016), and the Coastal Dune Model (Durán and Moore, 2013) 153 to coevolve the nearshore, beach, and dune in response to both subaqueous and 154 subaerial sediment transport (Cohn et al., 2019a; Itzkin et al., 2022). Windsurf can be 155 used to test a range of boundary conditions related to ecomorphodynamic processes to 156 explore the relative influence of different factors on foredune morphology and its change 157 (Ruggiero et al., 2019). Windsurf was initially developed and tested with reasonable skill 158 for a wide, dissipative beach on the west coast of the U.S. over a one-year period (Cohn 159 et al., 2019a). More recently, Windsurf has been used to reproduce hindcasts of beach

160 evolution and vertical dune growth over a one-year period at two field sites on Bogue 161 Banks, a barrier island in North Carolina, U.S. (Itzkin et al., 2022). The study of Itzkin et 162 al. (2022) included management scenarios for dunes with and without sand fences. 163 In this study, we initially quantify dune morphology and its interannual change 164 along Cape Lookout National Seashore (CALO, North Carolina, USA). We then 165 investigate the relative influence of factors that are likely to affect rates and types (i.e., 166 incipient dune development, widening of the dune, and/or vertical accretion) of foredune 167 growth using Windsurf. Our specific research questions are:

168 1) What are the observed temporally and spatially varying rates and 169 characteristics of foredune morphological change along our study region?

170 2) What are the relative contributions of key factors, including pre-existing 171 morphology, environmental wind and hydrodynamic forcing conditions, sediment grain 172 size distribution, and minimum vegetation elevation, to foredune growth in this region? 173 We first quantified foredune changes using annually collected in-situ 174 geomorphological measurements from 2016-2019. These data, along with in-situ 175 ecological observations and environmental conditions (e.g., water level, wave, and wind 176 data) compiled from hindcast and observed data, were incorporated into Windsurf and 177 used to produce a one-year hindcast of dune growth at a diagnostic field site. We then 178 used the calibrated model to explore and quantify the relative influence of pre-existing 179 morphology, environmental forcing conditions, sediment, and ecological characteristics 180 at the annual timescale via two distinct numerical modeling experiments: one using 181 observations from four field sites along CALO that exhibited different rates and types of 182 foredune growth and one using the full range of foredune growth factors observed within

183 our entire study area. We calculated changes from the initial and final modeled 184 response variables (i.e., dune toe elevation, dune crest elevation, and sediment volume 185 above a contour) to evaluate how different factors within the model affected dune 186 growth. This work aims to improve our understanding of foredune growth and recovery 187 processes and provides insights for modeling coastal change, predicting coastal hazard 188 vulnerability, and guiding coastal adaptation strategies including dune grading, dune 189 grass planting, and beach nourishment projects.

190 2.

Methodology

191 2.1. Study Area, Field Observations, and Other Datasets

192 Cape Lookout National Seashore (CALO) is located in North Carolina on the U.S. 193 Atlantic Coast and consists of three barrier islands: Shackleford Banks (SHB), South 194 Core Banks (SCB), and North Core Banks (NCB) (Figure 1). This region was 195 established as a National Seashore in 1966 and is managed by the U.S. National Park 196 Service. As such, CALO is minimally impacted by humans compared to more developed 197 areas on the Outer Banks barrier islands. The CALO coastline exhibits spatial variability 198 in beach and dune morphology, wind and wave climate, sediment characteristics, and 199 dune grass composition and density, making it ideal to investigate for our study (Dolan 200 and Lins, 1985; Godfrey, 1977, 1976; Goldstein et al., 2018; Hacker et al., 2019; 201 Hovenga et al., 2021, 2019; Jay et al., 2022; Riggs and Ames, 2007; Stockdon and 202 Thompson, 2007).



203

204 Figure 1. Cape Lookout National Seashore (North Carolina, USA) is comprised of three 205 barrier islands: Shackleford Banks (SHB), South Core Banks (SCB), and North Core 206 Banks (NCB). Markers indicate the 55 field sites (1-12 on SHB, 0-20 on SCB, and 1-22 207 on NCB) where topographic, sediment and vegetation data were collected. Marker 208 colors indicate the interannual dune volume change (m³/m) between surveys from 209 2016-2017, 2017-2018, and 2018-2019 moving seaward. Arrows show the locations of 210 the SCB5, SHB8, SCB1, and NCB17 field sites. The bottom right plots show the 211 probability density function (PDF), mean (μ), and standard deviation (σ) of the 212 interannual volume change for all 55 field sites. The top left inset shows the locations of 213 the National Oceanic and Atmospheric (NOAA) weather station (CLKN7), NOAA tide

gauge (8656483), and United States Army Corps of Engineers (USACE) Wave
Information Studies (WIS) stations (63268, 63272, and 63287).

216 Beach and dune change along CALO was quantified using Real Time Kinematic 217 Global Positioning System (RTK-GPS) techniques to measure annual in-situ 218 topographic profiles along transects in the cross-shore direction. Additionally, surface 219 sediment samples were collected at the dune toe and sieved to obtain grain size 220 distributions. Vegetation characteristics were measured along the dune profile at each 221 site, including grass density and a measure of minimum vegetation elevation, using the 222 methods of Hacker et al. (2019) and Jay et al. (2022). These datasets were obtained at 223 55 field sites (12 on SHB, 21 on SCB, and 22 on NCB) annually in the fall of 2016-2019 224 (Figure 1; Table 1). NCB was not surveyed in 2019 due to the extensive overwash that 225 occurred during Hurricane Dorian, resulting in unsafe field conditions. Foredune 226 morphometrics, including the dune toe, crest, and heel, were extracted from the field 227 measured cross-shore profiles using a manual delineation and interpretation approach 228 (Fabbri et al., 2017; Lentz and Hapke, 2019). The dune volume was calculated between 229 the seaward-most two-meter contour of the profile and the cross-shore location of the 230 2016 dune heel. All vertical references in this study are relative to the North American 231 Vertical Datum of 1988 (NAVD88), which is 0.11 m above mean sea level (MSL) at the 232 nearest tide gauge (Station: 8656483; NOAA, 2020a) (Figure 1). Note that total vertical 233 uncertainty (i.e., arising from GPS, calibration, and repeatability errors combined in 234 guadrature) associated with RTK-GPS methods is typically less than 8 cm (Ruggiero et 235 al., 2005). The measured topography was merged with bathymetry from the National 236 Centers for Environmental Information (NCEI) digital elevation model (DEM) to extend

the profiles to approximately the nine-meter water depth contour (NOAA, 2016).

238 Foreshore beach and shoreface slopes were calculated at MSL and the -6 m elevation

contour, respectively, by fitting a linear regression to the profile at each contour location

within ±5 m in the cross-shore direction. A definition sketch of the extracted beach and

- foredune morphometric features are provided in Hovenga et al. (2021).
- Table 1. Collection dates and type of in-situ datasets collected at the three barrier

243 islands: Shackleford Banks (SHB), South Core Banks (SCB), and North Core Banks

244 (NCB) (Figure 1). Dataset types include cross-shore topographic profiles (topo),

sediment samples collected at the dune toe, and vegetation measurements.

Dataset	Dates	Barrier Island	Dataset Type
2016	10/18-25/2016	SHB, SCB, NCB	Topo, sediment, vegetation
2017	10/14-20/2017	SHB, SCB, NCB	Topo, sediment, vegetation
2018	10/09-17/2018	SHB, SCB, NCB	Topo, vegetation
2019	11/10-13/2019	SHB, SCB	Topo, vegetation

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Environmental conditions including wave height, period, and direction were
acquired from USACE WIS hindcasts (U.S. Army Corps. of Engineers, 1997) (Figure 1).
Wind speed and direction were acquired from the NOAA CLKN7 weather station
(NOAA, 2020b) (Figure 1). Water level data was acquired from the NOAA tide gauge
8656483 (NOAA, 2020a) (Figure 1). The varying shoreline orientation within CALO
influences the environmental forcing conditions experienced at each field site due to
sheltering effects.

254 2.2. Windsurf Modeling Approach

255 We used the coupled numerical model Windsurf to simulate coastal profile 256 evolution in response to marine- and aeolian-driven sediment transport (Cohn et al., 257 2019a). The modeling framework communicates model outputs (i.e., morphology, water 258 levels, and bed shear stress) between the standalone model cores XBeach (release 259 1.23), Coastal Dune Model (CDM; release 1.0), and Aeolis (version 1.1.0). We first 260 calibrated Windsurf for the SCB5 field site (Figure 1) using in-situ geomorphological and 261 ecological observations combined with hourly water level, wave, and wind data. The 262 model was then used to explore and quantify the relative influence of pre-existing morphology (i.e., topo-bathymetric profiles), environmental forcing conditions (i.e., wave 263 264 and wind climate due to the varying shoreline orientation), sediment (i.e., median grain 265 size, D_{50} , and distribution represented by D_{10} , D_{50} , and D_{50}) and ecological (i.e., 266 minimum vegetation elevation) characteristics via two distinct numerical modeling 267 experiments.

268 2.3. Model Calibration Procedure

Using observed conditions from 2016 to 2017 at field site SCB5 (Figure 1), we calibrated Windsurf at the annual scale by optimizing parameters related to the individual cores: Aeolis (i.e., the aeolian sediment transport coefficient, Cb) and XBeach (i.e., skewness factor, facSk, and asymmetry factor, facAs) (Figure 1; Table 2). We selected SCB5 because the high rate of vertical crest accretion and volumetric growth at this site encompassed the range of changes observed elsewhere (Section 3.1).

275 Table 2. Key calibration model parameters, range of tested values, and final calibrated

values for the Windsurf model at the SCB5 field site (Figure 1). The model was

277 calibrated using error metrics 1-8, and the error values for the final, one-year calibrated

278 model are provided for each error metric.

Model Pa	rameter	Model Core	Min Value	Increment	Max Value	Calibrated Value
Cb		Aeolis	0.1	0.1	0.3	0.3
facSk		XBeach	0	0.1	0.7	0.5
facAs		XBeach	0	0.1	0.7	0.2
Error Metrics			Error Value			
(1) Dune) Dune volume (m ³ /m)			-0.32		
(2) Dune	2) Dune crest elevation (m)			-0.05		
(3) Bed e	Bed elevation at the 2016 dune toe cross-shore location (m)			0.16		
(4) Root seaw	Root Mean Square Error (RMSE; m; computed between the observed 2017 seaward- and landward-most points)			0.16		
(5) RMS locat	RMSE for the dune (m; measured between the 2016 dune toe cross-shore location and the observed 2017 landward-most point)			0.12		
(6) Brier comp	Brier Skill Score (BSS [Murphy and Epstein, 1989; Sutherland et al., 2004]; computed between the observed 2017 seaward- and landward-most points)			0.96		
(7) Bed e	Bed elevation change at the 2.1 m depth (m)			1.18		
(8) Bed e	Bed elevation change at the 6.5 m depth (m)			-0.60		

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280 We ran 192 simulations using every combination of Cb, facSk, and facAs for the 281 values listed in Table 2 while all other model parameter settings were set to default 282 values. Note that a morphological acceleration factor (MORFAC) of 5 was used in 283 XBeach after preliminary testing showed this value reduced model run time without 284 significant change to model responses. Model responses were evaluated using values 285 for the error metrics provided in Table 2. Error metrics 1-6 were calculated between the 286 final 2017 modeled profile and 2017 observed profile. For example, error metric (1) 287 dune volume is equal to the 2017 modeled dune volume minus the 2017 observed dune 288 volume. Error metric 6 represents the Brier Skill Score (BSS) (Murphy and Epstein, 289 1989; Sutherland et al., 2004). Additionally, we computed the bed elevation change

between the initial and final modeled profiles at two offshore depths (Error metrics 7 and 8); since no nearshore bathymetric change was measured for this study, these metrics were minimized for the smallest bed changes at the 2.1 and 6.5 m depths. The individual model runs were ranked by each error metric from best (largest BSS and smallest absolute minimum error for all other metrics) to worst (smallest BSS and largest absolute maximum error for all other metrics). We then computed two composite error scores, CompErr₆ and CompErr₈, using the following:

297
$$CompErr_n(m) = \sqrt{\frac{\sum_{i=1}^{n} rank_err_i^2}{n}}$$
(Eq 3.1)

298 where $CompErr_n(m)$ is the composite error score for each model run, m. Each 299 composite error score is computed using *n* number of error metrics and *rank_err* is the 300 model simulation rank for each individual error metric, *i* (Table 2). CompErr₈ (computed 301 from error metrics 1-8) was used to assess errors holistically across the nearshore, beach, and dune, while CompErr₆ (computed from error metrics 1-6) was used to finely 302 303 assess the model performance across the beach and dune, which is the focus of this 304 study. The final calibrated parameters Cb, facSk, and facAs were selected using the 305 model simulation that scored best for both CompErr₆ and CompErr₈. Although we used 306 a manual calibration approach, other more automated calibration methods such as 307 those that utilize machine learning techniques (e.g., Goldstein and Moore, 2018 and 308 Itzkin et al., 2022) may improve results but are beyond the scope of this study.

309 2.4. Modeling Experimental Design

310 We developed two 1D numerical modeling experiments to assess foredune 311 responses to variations in the factors that are likely key influencers of foredune growth. 312 Both modeling experiments focus on one year of data (2016–2017); this time period 313 was selected because observations revealed significant alongshore variations in 314 foredune growth rates and foredune growth types during this time window. For 315 Experiment 1, the in-situ factors at four field sites (i.e., SCB5, SHB8, SCB1, and 316 NCB17; Figure 1) were tested independently in Windsurf (Table 3). We chose these 317 four sites because they exhibited different rates and types of foredune growth. 318 Boundary conditions and all other model parameters remain unchanged from the 319 calibrated SCB5, or 'baseline model' except for those shown in bold in Table 3. For 320 example, Run 1.8 used the sediment size (D₁₀, D₅₀, D₉₀) measured at the SHB8 field 321 site and all other dune growth factors remained unchanged from the baseline model. 322 Table 3. Modeling design for Windsurf Experiment 1. Run 1.1 is the calibrated SCB5 323 (baseline) model, which uses all the dune growth factors (pre-existing morphology, 324 environmental conditions, sediment size, and minimum vegetation elevation) observed 325 at the SCB5 field site. Runs 1.2-1.13 use different pre-existing morphology (Runs 1.2-326 1.4), environmental conditions (Runs 1.5-1.7), sediment size (Runs 1.8-1.10), and 327 minimum vegetation elevation (Runs 1.11-13) boundary conditions that represent 328 observations at the SHB8, SCB1, and NCB17 field sites. The bold text signifies which

329 dune growth factors differ in each model run compared to the baseline model.

Run Number	Pre-existing Morphology	Environmental Conditions	Sediment Size D ₁₀ , D ₅₀ , D ₉₀ (mm)	Minimum Vegetation Elevation (m)
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1.1 (Baseline)	SCB5	SCB5	0.16	0.25	0.38	3.0
1.2	SHB8					
1.3	SCB1	SCB5	0.16	0.25	0.38	3.0
1.4	NCB17					
1.5		SHB8				
1.6	SCB5	SCB1	0.16	0.25	0.38	3.0
1.7		NCB17				
1.8 (SHB8)			0.20	0.31	0.53	
1.9 (SCB1)	SCB5	SCB5	0.23	0.43	1.06	3.0
1.10 (NCB17)			0.16	0.24	0.40	
1.11 (SHB8)						2.9
1.12 (SCB1)	SCB5	SCB5	0.16	0.25	0.38	2.1
1.13 (NCB17)						2.1

330 In Experiment 2, we modeled foredune response with Windsurf from 2016-2017 331 using the full range of foredune growth factors (i.e., environmental forcing conditions 332 dictated by the shore-normal angle, median grain size, and minimum vegetation 333 elevation) observed within CALO (Table 4). We used the calibrated SCB5 model and 334 only varied those parameters shown in Table 4. Shore-normal angles were measured in 335 degrees using a nautical convention (i.e., the angle from where onshore is directed, 336 measured clockwise from geographic North. For example, a shore-normal angle of 135 337 degrees would represent an onshore direction from the southeast to the northwest, a 338 fairly typical shore-normal angle for NCB). For Runs 2.1-2.6, we tested a range of 339 shore-normal angles from 100 to 250 degrees, increasing the shore-normal value by 30 340 degrees between each run (Table 4). These values represent the range of shore-normal 341 angles measured at all 55 field sites within CALO (101 to 255 degrees; Table 4). For 342 model Runs 2.1-2.6, we used the environmental conditions that would be experienced 343 at a location for each specified shore-normal angle (Table 4; described in more detail 344 below).

Table 4. Modeling design for Windsurf Experiment 2. We tested the full range of dune

346 growth factors observed within CALO including the environmental conditions dictated by

- the shore-normal angle, median sediment grain size, and minimum vegetation
- 348 elevation.

Run Number	Factors	Values	Observed CALO Range
2.1		100	
2.2	Environmental Conditions (Shore-normal angle, degrees)	130	CALO Min = 101 CALO Max = 255
2.3		160	SCB5 = 115
2.4		190	SHB8 = 207
2.5		220	SCB1 = 249 NCB17 = 138
2.6		250	10017 - 100
2.7	Median Sediment Grain Size (D ₅₀ , mm)	0.15	
2.8		0.20	CALO Min = 0.17
2.9		0.25	CALO Max = 0.44
2.10		0.30	SCB5 = 0.25 SHB8 = 0.31
2.11		0.35	SCB1 = 0.43
2.12		0.40	NCB17 = 0.24
2.13		0.45	
2.14		1.0	
2.15	Minimum Vegetation Elevation (m)	1.5	CALO MIN = 0.9 CALO Max = 6.6
2.16		2.0	SCB5 = 3.0
2.17		2.5	SHB8 = 2.9
2.18		3.0	SGB1 = 2.1 NCB17 - 2.1
2.19		3.5	

349

Pre-existing morphology was implemented within the model as a 1D cross-shore profile. Cross-shore grid spacing varied from 20 m offshore to 1 m onshore of the -1 m contour. Increasingly finer grid resolution had minimal impact on the model results yet added significant computational time.

- To account for the varying wind and wave environmental forcing conditions experienced at the SCB5, SCB1, NCB17, and SHB8 field sites, the onshore (shore-
- 356 normal) angle was measured perpendicular to the average alongshore orientation at

357 each of the field sites. The range of environmental forcing scenarios was implemented 358 within Windsurf by pre-processing the input wind and wave directions to include the 359 shore-normal components ± 90 degrees at SCB5, SCB1, NCB17, and SHB8 (Runs 1.1, 360 1.5-1.7 in Experiment 1) and for the shore-normal angles in Runs 2.1-2.6 in Experiment 361 2 (Table 4). Note, this filtering method did not violate the model coordinate system. 362 These model runs were used to explore how the environmental conditions experienced 363 at different locations within CALO may influence dune growth. Windsurf distinguishes 364 between marine-driven (XBeach) and aeolian-driven (Aeolis) sediment transport which 365 is explored within Experiment 2.

366 Sediment grain size characteristics are represented in the model core Aeolis by 367 D_{10} , D_{50} , and D_{90} . These values were extracted from the full distributions of the collected 368 sediment samples. Aeolis can simulate multi-fraction sediment transport incorporating 369 sorting and armoring processes using a full grain size distribution (Hoonhout and de 370 Vries, 2016). However, we used a three-fraction, cross-shore uniform bed layer for 371 faster computational processing. In Experiment 1, we used the sediment grain size 372 distributions (D₁₀, D₅₀, and D₉₀) measured from the SCB5, SHB8, SCB1, and NCB17 373 field sites (Runs 1.1, 1.8-1.10). For Experiment 2, we used sediment grain sizes D₁₀ and 374 D_{90} measured at the SCB5 site and only varied the median grain size (D_{50}) in the model. 375 The CDM model core of Windsurf computes spatially varying bed shear stress 376 due to the presence of vegetation above a specified elevation and includes a linear 377 growth rate for the fraction of vegetation cover. Within Windsurf, the vegetation limit is 378 fixed at a vertical contour (minimum vegetation elevation) rather than at a fixed cross-379 shore location so as to allow for horizontal migration of the dune that could change the

beach width (Cohn et al., 2019a). In this study, we explored the effect of minimum
vegetation elevation in our model runs. Although other vegetation characteristics such
as growth rate, plant density, and aboveground and belowground biomass have been
shown to influence dune morphology (Biel et al., 2019; Bryant et al., 2019;
Charbonneau et al., 2021; Feagin et al., 2015; Hacker et al., 2019; Hesp, 1989; Hesp et
al., 2019; Jay et al., 2022; Zarnetske et al., 2015, 2012), exploration of these
parameters in the model or the data sets was beyond the scope of this study.

387 **3. Results**

388 3.1. Observed Variability in Interannual Rates and Characteristics of Dune 389 Evolution

390 Field measurements of cross-shore profiles at four representative field sites, 391 SCB5, SHB8, SCB1, and NCB17, show highly variable dune evolution from 2016-2019, 392 and illustrate the variation in rates and characteristics of change observed within CALO 393 (Figure 1; Figure 2). For example, from 2016-2017, the foredune at SCB5 accreted 394 vertically but then was overtopped and lost significant volume by 2018. It then began to 395 show recovery by 2019, with foredune building occurring approximately 20 meters 396 landward of the initial dune crest position. In contrast, the foredune at SHB8 remained 397 relatively stable from 2016-2019. Erosion occurred on the beach and at the dune toe, 398 resulting in a vertical scarp at the base of the dune. Likewise, the foredune at SCB1 had 399 minimal vertical dune growth, but dune volume increased due to horizontal growth on 400 both the seaward and landward sides of the dune crest. Finally, the foredune at NCB17, 401 which was in an area that was overwashed prior to 2016, grew rapidly on its seaward

side. At these four sites, dune volume change ranged interannually from 0.9 to 10.6



403 m³/m in 2016-2017, -21.0 to 13.1 m³/m in 2017-2018, and 0.0 to 5.4 m³/m in 2018-2019.

Figure 2. Observed variation in rates and characteristics of dune evolution at four field sites: SCB5, SHB8, SCB1, and NCB17 (Figure 1). Changes in the dune volume (Δ Vol) and crest elevation (Δ Crest) are computed interannually. The vertical, black dotted line represents the 2016 dune heel and landward-most extent used to calculate dune volume change. The squares show the measured minimum vegetation elevation and its cross-shore location on the profile for each year. NCB17 was not surveyed in 2019 due to unsafe field conditions caused by Hurricane Dorian.

412 Dune volume changes computed for all 55 field transects in CALO showed 413 spatially and temporally varying response from 2016-2019 (Figure 1). Dune volumes 414 increased by an average of 2.9 (standard deviation, σ =5.4) from 2016-2017 and by 1.6 415 (σ =9.1) m³/m from 2018-2019 (Figure 1). Widespread erosion occurred across all 416 islands from 2017-2018 (mean, μ =-11.9 m³/m), with some sites eroding by as much as 417 20 m³/m. This significant erosion is attributed to Hurricane Florence, which passed 418 south of CALO in mid-September of 2018, approximately one month prior to our field 419 data collection (NOAA, 2018). The period from 2017-2018 also resulted in the greatest 420 variability in dune volume change (σ =12.8 m³/m). Despite the widespread erosion that 421 occurred within much of CALO during this period, the northern-most region of NCB 422 increased in volume.

423 During the study period, changes occurred at the dune toe cross-shore location 424 and the dune toe and crest elevation. Changes in these metrics were plotted against 425 each other (Figure 3) to show the varying characteristics of dune change that occurred. 426 We classified dune change in terms of horizontal progradation (Quadrants (Q) I and IV) 427 and retreat (QII and QIII) and vertical accretion (QI and QII) and erosion (QIII and QIV) 428 (Figure 3). Profiles within Quadrant IV exhibited an inverse relationship between dune 429 toe elevation and cross-shore location, where dune toe progradation coincided with 430 erosion (Figure 3a). The majority of dune toe retreat and erosion occurred from 2017-431 2018 (Figure 3a, QIII). In contrast, many profiles prograded and accreted at the dune 432 toe from 2016-2017 (Figure 3a, QI). The relationship between dune toe location and 433 dune crest elevation change was also variable (Figure 3b). Dune crest accretion 434 occurred at profiles that experienced progradation and retreat at the dune toe (Figure 435 3b, QI and II). However, dune crest erosion combined with toe retreat were the most prevalent characteristic of dune evolution from 2017-2018 (Figure 3b, QIII). Note that 436 437 incipient dune formation did not occur at any of the field sites between 2016-2019.



Figure 3. Relationship between the interannual change (2016-2017, 2017-2018, and
2018-2019; represented by the different colors) in dune toe cross-shore location and (a)
dune toe elevation and (b) dune crest elevation. Quadrants (QI-IV) represent different
characteristics of dune change (i.e., progradation and retreat of the dune toe crossshore location and erosion and accretion of the dune toe and crest elevation).

444 **3.2.** Variability in Foredune Growth Factors

445 **3.2.1. Pre-existing Morphology**

446 Cross-shore topographic profiles at the SCB5, SHB8, SCB1, and NCB17 field 447 sites in 2016 showed differing pre-existing morphologies (Figure 2; Figure 4). The dune 448 at SCB1 was the tallest (5.2 m) followed by SHB8 (4.7 m). The crest heights on SCB5 449 and NCB17 were both approximately 3.6 m. Dune toe elevations were also lower at 450 SCB5 and NCB17 compared to SCB1 and SHB8. SHB8 had the steepest foreshore 451 beach and dune face slopes, narrowest beach width, and largest dune volume of all four 452 profiles. The dune at NCB17 was fronted by the widest, shallowest beach. At the MSL 453 contour (-0.11 m), the beach was shallowest at NCB17 (0.021 m/m), and steepest at

454 SCB5 (0.063 m/m) (Figure 4). At the -6 m contour, the shoreface was shallowest at 455 SCB1 (0.004 m/m) and steepest at NCB17 (0.035 m/m).



Figure 4. Observed 2016 beach and dune topography at SCB5, SHB8, SCB1, and
NCB17 sites (Figure 1), merged with bathymetry from the National Centers for
Environmental Information (NCEI) digital elevation model (DEM). Profiles have been
aligned at the mean sea level (MSL) contour (-0.11 m) to emphasize morphological
differences.

462 **3.2.2. Environmental Forcing Conditions**

Wave hindcasts from the offshore WIS station nearest to each of the four field sites (63272 for SCB5, 63287 for SHB8 and SCB1, and 63268 for NCB17) revealed that the October 2016-2017 dominant wave direction was from the southeast (mean of all three WIS stations, μ =141.8° and σ =61.3°. Wave direction is reported in degrees relative to a nautical convention, e.g., the direction waves come from, measured clockwise from geographic North). The average wave height was 1.3 m (σ =0.6 m) and the average peak wave period was 7.5 sec (σ =2.3 sec). The last two months of the

470 environmental timeseries (i.e., 08-09/15/17 and 09-10/15/2017) showed increased wave 471 heights and longer wave periods (Figure 5b,d), which are attributed to multiple storms 472 that passed within a 500 km radius of CALO during this period including an unnamed 473 tropical storm (Aug. 27-29), Hurricane Gert (Aug. 12-18), Hurricane Jose (Sept. 4-25), 474 and Hurricane Maria (Sept.16-Oct. 2) (NOAA, 2018). The dominant wind direction, 475 observed at the NOAA CLKN7 weather station from 2016-2017, was from the northeast 476 and southwest and the average windspeed was 5.6 m/s (σ =2.7 m/s). The 2016-2017 477 wave and wind characteristics did not differ substantially from multi-decadal trends (not 478 shown). The multi-decadal (1980-2019) dominant wave direction was also from the 479 southeast (μ =132.1° and σ =52.6°), and the multi-decadal average wave height and 480 period were 1.2 m (σ =0.6 m) and 8.4 sec (σ =2.4 sec), respectively. The multi-decadal 481 (1997-2019) dominant wind direction was also from the northeast and southwest and 482 the average windspeed was 5.7 m/s (σ =2.9 m/s).

483 Within the entirety of CALO, the shore-normal angle ranged from 101-255° 484 (Table 4). At the SCB5, SHB8, SCB1, and NCB17 field sites, the shore-normal angle 485 ranged from 115-207° (Table 4). The offshore WIS station nearest to each of the four 486 field sites showed the wave height and period varied minimally among the WIS stations 487 from October 2016 to 2017 (Table 1; Figure 1; Figure 5b,d); the most significant 488 difference was the onshore wave direction (Figure 5c). Note that in Figure 5c, the wave 489 directions experienced at all four sites have been oriented to use 0° as the onshore 490 wave direction, rather than the site-specific shore-normal angle, to allow better 491 comparison of onshore directed waves among the four sites. SCB5 and NCB17 were 492 more exposed to onshore directed waves, with 87% and 91% of waves, respectively,

directed within ± 90° of shore-normal. In contrast, only 67% (SHB8) and 39% (SCB1) of the hourly wave conditions were oriented onshore for the other two sites. However, the average wave height of onshore directed waves (1.2-1.3 m) did not vary significantly among the four field sites. The cross-shore component of the wind velocity, calculated from the NOAA CLKN7 weather station, varied with time and field site due to the varying shoreline orientation (Figure 5e). The average cross-shore wind velocity was larger at SHB8 (4.0 m/s) and SCB1 (3.6 m/s) and smaller at SCB5 and NCB17 (2.4 m/s at both).



501 Figure 5. Time series of environmental forcing variables from October 2016-2017. (a) 502 Still water level (SWL) from NOAA tide gauge 8656483, (b) wave height, (c) wave 503 direction, and (d) wave period from USACE WIS stations (63272, 63287, and 63268), 504 and (e) onshore wind velocities from NOAA weather station CLKN7. The colors 505 represent wave and wind data from the WIS stations located nearest the field sites: 506 SCB5 (63272), SHB8 (63287), SCB1 (63287), and NCB17 (63268) (Figure 1). The 507 onshore wave and wind data at each field site are shown. The onshore wave direction 508 relative to each field site is represented by 0° in panel c.

509

3.2.3. Sediment Grain Size Distribution

510 Within CALO, the median sediment grain size varied from 0.14-0.44 mm (Figure 511 6). Larger grain sizes were observed along the east-west oriented shorelines of SHB 512 and southernmost region of SCB. Sediment sorting values tended to vary with median 513 grain size; poorer sediment sorting occurred at sites with larger median grain sizes. At 514 the SCB1, SCB5, NCB17 and SHB8 field sites, the median sediment grain sizes ranged 515 from 0.24-0.43 mm, and classified as moderately to moderately well sorted (Table 3, 516 Figure 6) (Folk, 1968; Folk and Ward, 1957; Pettijohn et al., 1987). SCB5 and NCB17 517 had similar median sediment grain sizes (0.25 and 0.24 mm, respectively) and sorting 518 values (0.5 phi; moderately well sorted). SCB1 had the coarsest median grain size (0.43 519 mm) and the most poorly sorted distribution (0.9 phi; largest sorting value).



Figure 6. Sediment grain size and minimum vegetation elevation at all 55 field sites in the Cape Lookout National Seashore, NC study region. Median grain size (D₅₀, mm; represented by the circles) and sorting (phi; represented by the triangles) are from 2016 (SCB1 and SCB5) and 2017 (all other sites). The minimum vegetation elevations (squares) are from 2016. Marker colors indicate the values of the sediment grain size and minimum vegetation elevation. The top left inset shows the location of CALO relative to the U.S. Atlantic coast.

528 3.2.4. Minimum Vegetation Elevation

529 The average minimum vegetation elevation from 2016-2019 along all CALO field 530 sites was 3.1 m (σ =0.9 m) and ranged from 0.9 m to 6.6 m (Table 4). The average 531 minimum vegetation elevation in 2016 was 2.9 m (σ =0.8 m) and ranged from 1.1 m to 4.8 m (Figure 6). The minimum vegetation elevation gradually increased at more
northernly latitudes and was, on average, higher on NCB than on SCB and SHB (Figure
6). At the SCB5, SHB8, SCB1, and NCB17 field sites, the minimum vegetation elevation
was 3.0 m, 2.9 m, 2.1 m, and 2.1 m, respectively (Table 3; Figure 6). For additional
information on vegetation measurements including distribution, abundance, and density
of dune grass species in CALO refer to Hacker et al. (2019) and Jay et al. (2022).

538 3.3. Windsurf Model Calibration

539 Windsurf was calibrated for one year (October 2016-2017) using SCB5 540 observations for the model parameters Cb, facSk, and facAs (Table 2). The observed 541 profiles from 2016 and 2017 showed sediment deposition on the beach, resulting in 542 increased bed elevation and shoreline progradation (Figure 7). During this time, the 543 dune volume increased by 10.9 m³/m and the dune crest elevation increased by 0.3 m. 544 The calibrated Windsurf model generally captured these observed changes, but slightly 545 underestimated the dune volume change by 0.32 m³/m and dune crest change by 0.05 546 m (Table 2; Figure 7). The modeled profile has a RMSE of 0.12 m and Brier Skill Score 547 of 0.96 (Table 2).



Figure 7. The coastal profiles at the SCB5 field site between 2016 and 2017 using a) observed (black) and Windsurf-calibrated (teal) bed elevations, and b) their change. Change in the dune volume (Δ Vol) and crest elevation (Δ Crest) reported in the legend were computed between the 2016 (observed) and 2017 (observed and calibrated) profiles.

3.4. Model Response to Variations in Factors Influencing Dune Growth

555 3.4.1. Experiment 1 Model Runs

556 The Experiment 1 modeling suite (Table 3) was run using the calibrated model 557 parameters and the observed pre-existing morphology, environmental forcing 558 conditions, sediment grain size, and minimum vegetation elevation at SCB5 (Run 1.1 559 baseline model). The values for each factor were then changed in the model one at a 560 time to represent observed conditions at the SHB8, SCB1, and NCB17 field sites. All other values in Windsurf were held constant across all of the simulations (Runs 1.2-1.13).

563 The simulations testing the influence of varying pre-existing nearshore, beach, 564 and dune morphology (Runs 1.1, 1.2-1.4) resulted in dunes that evolve at different rates 565 and exhibit different types of growth (Figure 8a). Run 1.3, which used the SCB1 pre-566 existing morphology, had the tallest initial dune crest and accreted at the dune crest by 567 0.5 m, more than any other profile. Run 1.4 (NCB17 pre-existing morphology) 568 developed an incipient dune seaward of the existing foredune at the 20 m cross-shore 569 location, which resulted in vertical growth of 1.1 m. Run 1.1 (SCB5 pre-existing 570 morphology, baseline simulation) had the most sediment deposition above the 2 m 571 contour. Run 1.2 (SHB8 pre-existing morphology), which had the steepest foreshore 572 beach slope and narrowest beach width of the four initial profiles, experienced the least 573 amount of sediment deposition above the 2 m contour and at the dune crest.

574 The simulations testing the environmental forcing conditions were varied 575 according to the shoreline orientation at each of the four field sites. Runs 1.1 and 1.7 576 used environmental conditions from SCB5 and NCB17, respectively, which are located 577 on east facing shorelines that are more exposed to the dominant wave direction (Figure 578 1; Figure 5). These model runs showed substantial sediment accumulation above the 2 579 m contour (Figure 8b). The bed elevation at the 30 m cross-shore location increased by 580 0.6 m for both model runs. Runs 1.5 and 1.6 used SHB8 and SCB1 environmental 581 conditions, respectively. These sites are more sheltered from wave action but are 582 exposed to the dominant cross-shore wind direction (Figure 5). In these model 583 simulations, sediment moved higher onto the beach (around 37 m in the cross-shore)

compared to the results of simulations testing the influence of pre-existing morphology.
The dune crest accreted 0.3 m for Runs 1.1 and 1.6 (SCB5 and SCB1 environmental
conditions, respectively) and 0.2 m for Runs 1.5 and 1.7 (SHB8 and NCB17
environmental conditions, respectively).

588 Variations in modeled beach and dune change due to variability in sediment 589 grain size were slight, especially relative to the influence of variability in the initial 590 morphology and environmental conditions (Figure 8c). The coarsest and most poorly 591 sorted sediment (Run 1.9; SCB1 sediment) produced the least dune crest growth. Finer 592 sediment (Run 1.1; SCB5 sediment and Run 1.10; NCB17 sediment) resulted in the 593 most accretion at the crest (0.3 m of vertical change for both simulations) and on the 594 seaward and landward side of the crest (not apparent at the scale shown in Figure 8c, 595 however the measured change between the 2016 observed and 2016-2017 modeled 596 Windsurf profile elevations at the cross-shore distance x=25 m and x=20 was 0.3 m and 597 0.1 m, respectively, for both Run 1.1 and Run 1.10). This resulted in a wider dune near 598 the crest and steeper dune face slope. Sediment from SHB8 (Run 1.11), which was 599 coarser than SCB5 (Run 1.1) and NCB17 (Run 1.10) but finer than SCB1 (Run 1.9), 600 resulted in relatively intermediate crest accretion and increased dune volume. 601 Simulations with lower minimum vegetation elevations (i.e., Run 1.12; SCB1 and 602 Run 1.13; NCB17) resulted in increased sediment accretion in front of the dune,

particularly near the 2.1 m contour where vegetation was present, thereby stunting
vertical dune growth landward of this contour (Figure 8d). Dunes with higher minimum
vegetation elevations (i.e., Run 1.1; SCB5 and Run 1.11; SHB8) developed taller dunes
that were wider near the crest.



608

Figure 8. Profiles for the observed elevations in 2016 and the Windsurf modeled profiles
(2016-2017) for each run in Experiment 1 using the varying a) pre-existing morphology,
b) environmental forcing conditions, c) sediment grain size (D₁₀, D₅₀, D₉₀), and d)
minimum vegetation elevation derived from in-situ values at the SCB5, SHB8, SCB1,
and NCB17 field sites (Table 3).

Modeled changes in the dune crest elevation and dune volume for each model run in Experiment 1 (Table 3) are shown in Figure 9. The dune crest elevation change varied most, within a range of 0.23 m, for simulations with varying pre-existing morphologies (Runs 1.1-1.4; Figure 9). The range of dune volume change was most influenced by changes in the environmental boundary conditions and varied by 7.8

619 m/m³ in Runs 1.1, 1.5-1.7. Minimum vegetation elevation had a larger effect on dune 620 crest elevation than sediment grain size, but varying sediment grain size resulted in 621 more dune volume change. Changes in the dune crest elevation and dune volume were 622 often synchronized among the varying boundary conditions, meaning that increases in 623 the crest relative to the baseline scenario coincided with increases in dune volume and 624 vice versa. Runs 1.3 and 1.4, which used the pre-existing morphology from SCB1 and 625 NCB17, respectively, were exceptions to this pattern. For these model runs, the dune 626 crest elevations increased relative to the baseline scenario and the dune volumes 627 decreased.





635 3.4.2. Experiment 2 Model Runs

The Experiment 2 modeling suite (Table 4) involved 19 simulations using the full range of observed foredune growth factors within CALO (2016-2017), including the environmental forcing conditions dictated by the shore-normal angle, median sediment grain size, and minimum vegetation elevation. Calibrated and all other model parameters were held constant among the model runs.

641 Of the factors tested in the Experiment 2 modeling suite, the environmental 642 forcing conditions dictated by the shore-normal angle produced the most variable 643 change in dune crest elevation and dune volume (Figure 10a,d). For shore-normal 644 angles between 100-130° (Runs 2.1-2.6), change in both the dune crest elevation and 645 dune volume decreased. The minimum change in these metrics occurred at 160° (Run 646 2.3) and then increased at progressively larger shore-normal angles (Runs 2.4-2.6). 647 Somewhat surprisingly, dune volume increase was greater for coastlines exposed to the 648 southeast (i.e., the dominant wave direction) as opposed to the southwest (i.e., the 649 dominant wind direction).

650 Model runs varying the median grain size (Runs 2.7-2.13) revealed that as 651 sediment grain size increased, dune crest elevation change and dune volume change 652 both decreased (Figure 10b,e). Likewise, as minimum vegetation elevation increased, 653 change in the dune crest elevation and dune volume increased (Figure 10c,f). At 654 elevations of 2.5 m and higher (Runs 2.17-2.19), the effect of the minimum vegetation 655 elevation on the coastal profile plateaued, and there was minimal change to the 656 response variables; change in the dune crest elevation and dune volume stabilized at 657 0.28 m and 10.6 m³/m, respectively. Comparing modeled results between the varying

median sediment grain size and minimum vegetation elevation factors (Runs 2.7-2.19),
the finest median sediment grain size (0.15 mm; Run 2.7) resulted in the greatest
positive change in dune crest elevation (0.31 m) and dune volume (11.2 m³/m). The

lowest minimum vegetation elevation (1.0 m; Run 2.14) resulted in no dune crest

662 elevation change (0 m) and the lowest change in dune volume (6.5 m³/m).



Figure 10. Change in the dune crest elevation (a-c; top row) and dune volume (d-f;
bottom row) from Experiment 2 using varying shore-normal angles that influence
environmental forcing conditions, median sediment grain sizes, and minimum
vegetation elevations (Table 4).

To further explore the marine and aeolian processes driving different beach and dune responses for the varying shore-normal angles shown in Figure 10a,d, the change in bed elevation associated with each of these processes is presented at the monthly

672 timescale (Figure 11). Marine- and aeolian-driven bed changes are defined as those 673 modeled in Windsurf's model cores, XBeach (marine) and Aeolis (aeolian). The total 674 monthly bed elevation change was influenced more by marine processes than by 675 aeolian processes at smaller shore-normal angles (e.g., 100° and 130°), which were 676 more exposed to the dominant southeast wave direction (i.e., μ =141.8°). Compared to 677 other shore-normal angles, 100° and 130° had larger marine-driven bed elevation 678 change rates which occurred at locations along the beach to the base of the dune (near 679 the 30 m cross-shore location). For the 100° and 130° shore-normal angles, the dune 680 crest (near the 20 m cross-shore location) accreted more as a result of aeolian-driven 681 transport. As shore-normal angles increased from 160° to 250°, and thus became more 682 sheltered from waves coming from the dominant direction and more exposed to the 683 southwest cross-shore wind direction, the monthly bed elevation change became more 684 influenced by aeolian processes. Interestingly, for these shore-normal angles (e.g., 160° 685 to 250°), the majority of the onshore migration of the pre-existing beach berm feature 686 (initially near the 55 m cross-shore location) resulted from aeolian transport rather than 687 marine transport (Figure 11). The shore-normal angle of 160°, which experienced the 688 least amount of change in dune crest elevation and dune volume (Figure 10a,d), was 689 oriented in neither the dominant wind nor wave direction. At this shore-normal angle, 690 both monthly marine and aeolian bed elevation changes were relatively smaller (Figure 691 11).

The change in monthly bed elevation also varied with time (Figure 11). For shore-normal angles of 100° and 130°, a large amount of sediment was deposited on the beach in the last two months of the simulation (i.e., 08-09/15/17 and 09-

695 10/15/2017). For sites with shorelines that were more sheltered from the dominant wave
696 action (i.e., 190-250°), there was no marine-driven bed elevation changes during this
697 time and aeolian-driven sediment transport was minimal. The largest monthly bed
609 elevation changes are sisted with a selien and import transport are used during the

- 698 elevation changes associated with aeolian sediment transport occurred during the
- 699 months of March to July.





- 702 second row), marine-driven bed elevation (ΔZb marine; third row), and total bed elevation (ΔZb total, aeolian- plus marine-
- 703 driven; fourth row) for each shore-normal (SN) angle from Experiment 2, Runs 2.1-2.6 (Table 4; columns). The bed

- elevation changes are shown at discrete cross-shore locations across the profile (x-axis), and the colors represent the
- 705 monthly timescale from October 2016-2017. The black dashed line beneath the colors in the figures in the top row (most
- visible in the top left plot) represents the initial profile.

707 4. Discussion

708 **4.1.** Relative Influence of Foredune Growth Factors

709 Of the four factors influencing foredune growth explored in this study, findings 710 from the suite of simulations in Experiment 1 indicate that the pre-existing morphology 711 of the beach and dune has the largest influence on subsequent dune evolution (Figure 712 8). The model results show that the pre-existing morphology alters the rates and types 713 of dune growth, especially the range of dune crest growth and the formation of incipient 714 dunes (e.g., Run 1.4). The pre-existing morphology is likely the most influential factor of 715 foredune change explored in this study because it encompasses many variables (e.g., 716 foreshore beach slope, shoreface slope, and beach width) that have been shown to 717 affect subaqueous and subaerial sediment transport, and thus dune change during 718 storms and recovery (Crapoulet et al., 2017; Héquette et al., 2019; Hesp and Smyth, 719 2016; Larson et al., 2004; Ruggiero et al., 2001; Sherman and Bauer, 1993; Short and 720 Hesp, 1982). For example, dune growth is smallest for the model simulation that used 721 the SHB8 morphology (Run 1.2); this is attributed to limited sediment transport rates to 722 the dune, caused by the narrow, steep beach at this site and thus larger runup and 723 restricted fetch length. The wider, shallower sloped beaches for the SCB5 (Run 1.1), 724 SCB1 (Run 1.3), and NCB17 (Run 1.4) morphologies result in lower runup, longer fetch 725 lengths, higher transport rates to the dune, and thus more dune growth.

The model simulations show that the rate of foredune growth, particularly the range of dune volume change, is most influenced by the environmental forcing conditions (Figure 8; Figure 10). We found that dune volume increases on shorelines

729 that are exposed to either the dominant wave direction or the dominant wind direction, 730 with larger change occurring for the former (Figure 11). The significant amount of 731 marine-driven beach deposition that occurred on east facing shorelines during the last 732 two months of the simulations (Figure 11) coincide with increased wave heights and 733 longer periods relative to the average 2016-2017 wave conditions (Figure 5). This is 734 attributed to multiple storms during this period including an unnamed tropical storm and 735 Hurricanes Gert, Jose, and Maria. These conditions resulted in taller dunes due to 736 increased sediment supplied by marine processes that was subsequently transported to 737 the dune crest via aeolian-driven transport. These conditions also resulted in dunes on 738 east facing shorelines that were greater in volume due directly to marine-driven 739 sediment transport to the base of the dune (above the 2 m contour) compared to the 740 south- southwest-facing shorelines that were more sheltered from wave action during 741 the period of study. These findings suggest that for certain hydrodynamic conditions 742 (i.e., elevated water levels, larger waves, and longer periods) and shoreline orientations, 743 marine processes may be a significant contributor to rapid and substantial foredune 744 growth. These model results are consistent with recent field data (Cohn et al., 2018) 745 and numerical modeling simulations (Cohn et al., 2019a) for dissipative beaches, which 746 have shown specific marine processes (i.e., infragravity swash, high still water levels, 747 and/or energetic wave conditions) can drive approximately 9%-38% of annual dune 748 growth. Similarly, these results are consistent with the positive, long-term relationship 749 found between foredune height and wave height (Durán and Moore, 2013; Hesp, 1988; 750 Miot da Silva et al., 2008; Moulton et al., 2021; Pellón et al., 2020; Ruggiero et al., 2005; 751 Short and Hesp, 1982).

752 Even though the hydrodynamic conditions during this study resulted in beach and 753 dune growth on exposed shorelines, more elevated water levels and energetic wave 754 conditions than those observed in our study period (such as those produced during 755 hurricanes and nor'easters) have the potential to erode and overtop dunes within this 756 region (Dolan and Lins, 1985; Hovenga et al., 2021; Passeri et al., 2020; Riggs and 757 Ames, 2007; Stockdon and Thompson, 2007). Our findings suggest that the future 758 resiliency of dune-backed coastlines in CALO will be affected by projected changes in 759 storminess patterns, shifts in the wave climate, and sea-level rise (Hicke et al., 2022; 760 Wang et al., 2004; Woolf et al., 2002). More research is needed to explore the 761 magnitude and frequency thresholds (Pellón et al., 2020) of marine-driven construction 762 and erosion of coastal dunes for present-day and projected future conditions.

763 Our model simulations show that dune crest elevation and dune volume both 764 increase as the median sediment grain size decreases; however, sediment grain size is 765 less influential in altering these foredune metrics compared to the other factors explored 766 in this study (Figure 9; Figure 10). For example, within CALO the range of observed 767 sediment grain sizes (0.17 mm to 0.44 mm) resulted in less dune crest elevation and 768 volumetric change than variations in both the minimum vegetation elevation and the 769 shore-normal angle, suggesting that sediment grain size is less influential in altering 770 foredune rate and type of growth in this region (Figure 10). However, the finest 771 sediment size investigated (0.15 mm) produced taller dunes and larger dune volumes 772 when compared to any of the observed minimum vegetation elevations within CALO. 773 This result suggests that the presence of very fine sediments could be an important 774 factor contributing to dune morphology.

775 The model simulations indicate that low minimum vegetation elevations can 776 hinder dune crest growth and limit sand volume change above the two-meter contour 777 (Figure 10). This is attributed to the reduced fetch length and increased drag of 778 vegetation at lower elevations, which limit aeolian-driven transport and cause sediment 779 to be deposited on the beach instead of in the dunes (Figure S1.1). For dunes that have 780 higher minimum vegetation elevations, sediment is eroded from the beach and 781 transported to the dune by aeolian-driven transport (Figure S1.1), resulting in more 782 dune accretion. Modeled morphometric changes plateaued as the minimum vegetation 783 elevation increased above 2.5 meters (Figure 10), indicating that the bed shear stress 784 reduction is maximized for all minimum vegetation elevations near the dune crest (2.5 m 785 and higher) and/or that, for these simulations, sediment availability or transport was 786 limited. The minimum elevation at which vegetation establishes on the dune, and thus 787 plant zonation, is related to the physiological tolerances of vegetation to sand burial and 788 seawater inundation (Du and Hesp, 2020; Hacker et al., 2012; Levin et al., 2008; Maun, 789 2009; Mullins et al., 2019; Seneca, 1972). A correlation between plant zonation and 790 beach type (dissipative vs. reflective) has been observed, in which increased foredune 791 heights are linked to wider plant zonation on dissipative beaches as a result of 792 decreased wave runup, salt spray, and sand salinity (Durán and Moore, 2013; Goldstein 793 et al., 2017; Hesp, 1988; Miot da Silva and Hesp, 2010; Saye et al., 2005; Weng et al., 794 1991). For our simulations on an intermediate beach (Section S1.2), we found that 795 lowering the minimum vegetation elevation and thus increasing the plant zonation 796 reduced the beach width and thus the fetch length such that sediment availability and

aeolian-driven transport was limited, ultimately resulting in shorter dunes that werewider near the base.

799 Although our findings are relevant at annual timescales, the relative importance 800 of foredune growth factors investigated here (and others not explored in this study such 801 as storm surge under sea-level rise, longshore transport gradients, armoring by 802 sediment sorting, and variable beach grass density) may change according to timescale 803 (seasonal to multi-decadal) (Carter, 1976; Carter and Rihan, 1978; Hoonhout and de 804 Vries, 2016; McKenna Neuman et al., 2012; Passeri et al., 2018; Roelvink and Costas, 805 2019; Zarnetske et al., 2015). When considering management of coastal dunes, our 806 findings suggest that management-based decisions which alter the pre-existing 807 morphology, such as beach and dune grading and beach nourishment, may have 808 considerable impacts on subsequent dune growth, particularly at annual timescales. 809 Additionally, the grain size selected for beach nourishment projects could influence 810 dune height and volume, such that the placement of sand that contains a greater 811 proportion of coarser grains than naturally found on the beach could reduce dune 812 growth. Finally, lowering the minimum vegetation elevation by planting further seaward 813 than naturally would occur may limit vertical dune growth.

814

4.2. Model Parameterizations and Assumptions

The numerical model used in this study, and the factors of variable dune growth that were tested here, include different parametrization schemes and assumptions that could affect simulated dune growth. For example, the 1D cross-shore modeling approach that we used in this study does not incorporate the higher dimensional variability of bathymetric/topographic features (e.g., 2D sandbars, troughs, and cusps,

820 and washover gaps in the dune line), all of which may influence dune evolution, 821 particularly "hot spot" erosional effects (Castelle et al., 2019, 2017; Houser, 2013; 822 Houser et al., 2008). Additionally, the variable environmental forcing conditions that we 823 employed are developed for each site using a filtering process to orient wave and wind 824 directions based on alongshore-averaged shoreline orientation. These wind and wave 825 conditions are imposed as model boundary conditions, along with a still water level 826 acquired from a single tide gauge. This approach simplifies or omits spatially varying 827 storm surge and sea level anomalies, refractive effects, and dissipation, which may 828 smooth or alter total water level variability along the shore (Serafin et al., 2019; 829 Theuerkauf et al., 2014). More research incorporating alongshore varying total water 830 levels developed via high fidelity hydrodynamic models is needed to understand the 831 influence these processes may have on dune growth. Lastly, process-based beach-832 dune evolution models, including Windsurf, typically include adjustable coefficients that 833 require calibration (Rafati et al., 2021). Additional testing is needed to explore the 834 variability of these parameters in Windsurf (e.g., Cb, facSk, and facAs) among different 835 field sites and determine the model's aptness at capturing all possible foredune change 836 (e.g., recovery and erosion) through time.

837 5. Conclusion

Annual field measurements in Cape Lookout National Seashore (CALO) showed temporal and spatial variability in foredune change including retreat / progradation and erosion / accretion. Model results using the coupled beach-dune evolution model Windsurf suggest that pre-existing morphology has the most significant influence on the type of foredune growth, which can vary from the development of incipient dunes to

horizontal and/or vertical change of existing dunes. Environmental forcing conditions
had the most influence on dune volume changes. Marine-driven sediment transport
were shown to drive rapid and significant dune accretion and progradation. The full
range of observed minimum vegetation elevations within CALO resulted in a larger
deviation of dune crest elevation and volume change compared to the full range of
observed median grain sizes.

849 Findings from this work may be used to inform coastal management decisions 850 such as dune restoration, grass planting, beach and dune grading, and beach 851 nourishment projects. By better understanding the ways in which important factors 852 influence dune growth, coastal managers may prioritize which, where, and how different 853 strategies are implemented. Within the scope of beach-dune modeling efforts, our 854 findings can be used to inform physics, parameterization schemes, and incorporate 855 management scenarios in numerical models (Itzkin et al., 2022; Ruggiero et al., 2019). 856 Additionally, findings from this work improve our understanding of foredune growth and 857 are significant to ongoing modeling efforts and field campaigns, coastal hazard 858 predictions, and resiliency planning.

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